

Both Part-A and Part-B are compulsory

Part-A (60 marks)

Answer all questions. Make suitable assumptions, and state them clearly

1) A 2100 MW, steam power plant has a thermal efficiency of 0.40. The plant uses coal which has a Heating Value of 24 MJ/kg and the combustion chamber operates with an air-fuel ratio of 15:1. A forced draft fan system used for maintaining the required air flow through the combustion chamber has to develop a fan total pressure rise of 480 Pa at an efficiency of 85%. The exhaust gas temperature at the entrance and exit of the chimney are 140°C and 110°C, respectively, while the average ambient air temperature is 21°C and pressure is 1.01 bar. The chimney height should be such that it develops a buoyancy pressure of 600 Pa. Assume: a) Density of air = 1.1 kg/m³, b) Specific heat, c_p of exhaust gases = 1.12 kJ/kg.K, c) Gas constant of air and exhaust gases = 0.287 kJ/kg.K. From the given data, find:

a) The power input to the forced draft fan system (in MW)

b) Height of the chimney (in m)

c) Heat loss from the exhaust gases in (MW) $\dot{m}_{exch} = ?$ $x=0$ $Q_r = \dot{m} \Delta x c_p h_{fg}$ (10)

2) The riser tube of a natural circulation, drum type boiler receives saturated liquid water at a velocity of 1.2 m/s from the downcomer. Water leaves the riser tube with an exit void fraction of 0.85 after absorbing 4.5 MW of heat from the furnace gases. The boiler operates at 160 bar. The saturated liquid and vapour densities at 160 bar are 585 kg/m³ and 108 kg/m³, respectively, and the latent heat of vapourization is 930 kJ/kg. At any section in the riser tube, the velocity of vapour is equal to 1.5 times that of the liquid. The riser tube has to be sized such that it develops a pressure rise of 32 kPa due to buoyancy. From the given data and using the equations given below, find a) the required riser diameter (in m), b) riser height (in m), and c) average heat flux in the riser tube (in kW/m²). (15)

The void fraction α is related to the dryness fraction x as: $\alpha = \frac{1}{1 + \left[\frac{(1-x)}{x}\right] \psi}$; where $\psi = \frac{\rho_g}{\rho_f} S$ and S is the slip ratio (ratio of vapour-to-liquid velocity). The average density of the two-phase mixture in the riser tube is given by: $S = 1.5$

$$\bar{\rho}_{2-\phi,R} = \bar{\rho}_f - \frac{(\bar{\rho}_f - \bar{\rho}_g)}{(1 - \psi)} \left\{ 1 - \left[\frac{1}{\alpha_e (1 - \psi)} - 1 \right] \ln \frac{1}{(1 - \alpha_e (1 - \psi))} \right\}$$

where α_e is the void fraction at the exit of the riser. Acceleration due to gravity (g) is 9.81 m/s².

3a) Superheated steam is expanded in a steam nozzle from an initial pressure and temperature of 120 bar and 400°C to a final pressure of 12 bar. Neglecting the velocity at the inlet to the nozzle, what should be the nozzle efficiency if the velocity required at the nozzle exit is 800 m/s? Use the data given in the table. (5)

t, °C	p, bar	x	h (kJ/kg)	s (kJ/kg.K)
400	120	-	3051	6.074
188	12	0	798.7 kg	2.217 kg
188	12	1	2784 kg	6.524 kg

$\eta = 1.3$

Lever Rule

3b) The above nozzle is connected to an impulse turbine at a nozzle exit angle of 12° . The inlet and exit blade angles of the turbine are 30° and 36° , respectively. Assuming frictionless flow through the turbine blades, find the power developed by the turbine in MW, if the mass flow rate of steam through the turbine is 12 kg/s . (10)

3c) Using suitable velocity diagrams and starting with Euler's turbo-machinery equation, prove that the specific work developed by a steam turbine with frictionless flow through blades is given by:

$$w = \frac{1}{2}(V_1^2 - V_2^2)$$

where V_1 and V_2 are the absolute velocities of steam at inlet and exit of the turbine blade. (5)

4a) Steam at a flow rate of 60 kg/s and 0.07 bar pressure (saturation temperature = 39°C and latent heat of vaporization = 2408 kJ/kg) at an inlet quality of 0.85 condenses on the shell side of a 2-pass, shell-and-tube type, power plant condenser. Cooling water ($c_p = 4.2 \text{ kJ/kg.K}$, $\rho = 1000 \text{ kg/m}^3$) from a cooling tower enters the condenser at 30°C and leaves at 35°C . Cooling water flows through the tubes which have an inner diameter of 25.4 mm and a wall thickness of 1.0 mm . The condensation heat transfer coefficient on the shell side is $3000 \text{ W/m}^2\text{K}$ and fouling resistance on water side is $0.0004 \text{ m}^2\text{KW}$. Heat transfer resistance of the tube wall is neglected. If from tube erosion point of view, the velocity of cooling water is to be restricted to 2.5 m/s , find the length of the condenser tubes. The heat transfer coefficient on cooling water side is equal to $4600 \text{ W/m}^2\text{K}$. (10)

4b) A natural draft cooling tower supplies cooling water to the above condenser. The condition of air at the inlet and exit of the cooling tower are: 35°C , 50% relative humidity ($W = 0.0178 \text{ kgw/kg a}$ & $h = 81 \text{ kJ/kg a}$) and 30°C and 100% relative humidity ($W = 0.0273 \text{ kgw/kg a}$ & $h = 100 \text{ kJ/kg a}$), respectively. Neglecting drift and bleed-off losses, find the make-up water requirement for the cooling tower in kg/h ? The enthalpy of make-up water is 120 kJ/kg . $m = 2.5 \frac{\pi D^2 L}{4}$ (5)

End of Part-A

Part-B (40 marks)

Answers should be brief and to the point. Drawings should be neat and clean with proper labels. Answer all questions. Make suitable assumption, wherever necessary.



5) (a) Draw backward, radial and forward curved vanes for a centrifugal impeller. Draw the velocity triangles on the diagram with proper labeling. (b) Derive the theoretical head (H) vs flowrate (Q) curve. Draw the theoretical pump characteristics for three blade angles. Assume whirl component at inlet is zero. (c) Step-by-step discuss the various losses occurring inside the impeller and finally obtain the actual pump characteristics curve. [3+3+4=10]

$$W = \frac{V_1^2 - V_2^2}{2(1-R)}$$

6) (a) Derive the relation between the ratio of kinetic to reaction component of energy with degree of reaction. (b) Find out the utilisation factor as a function of inlet flow angle and degree of reaction. (c) Derive speed ratio as a function of inlet flow angle and degree of reaction. Compare the speed ratio for fully impulse and 50% reaction machine. $\Phi = \frac{2 \cos \alpha}{1-R}$ [3+3+4=10]

7) (a) Draw schematic and velocity diagrams of compressor cascade and turbine cascade. (b) For axial flow machine, derive the degree of reaction as a function of the mean tangential component of relative velocity by drawing suitable velocity triangles and (c) Draw three separate diagrams to explain degree of reaction (i) zero, (ii) 1 and (iii) 0.5. $R = -\frac{V_{u \text{ mean}}}{u} \quad \Phi = u \cos \alpha / V_1$ [4+3+3=10]

8) A Kaplan turbine has a rated output of 2600 kW at 600 rpm , the head being 40 m of water. The velocity ratio is 1.25 . The overall and hydraulic efficiencies are 0.86 and 0.9 respectively. The hub diameter is 0.6 times the tip diameter, Calculate the (a) engineering specific speed, (b) tip diameter and hub diameter, (c) blade inlet and outlet angles at the tip, and (d) blade inlet and outlet angles at the hub. [1+3+3+3=10]

End of the Question Paper