

Q) The plastic behaviour of a metal cube expressed as ①

$$\bar{\sigma} = 500 \bar{\epsilon}^{0.5} \text{ MPa.}$$

Estimate the yield strength if a bar of this material is uniformly cold worked to a reduction of  $r = 0.3$

Ans:  $\epsilon = \ln \left[ \frac{1}{1-r} \right] = \ln \left[ \frac{1}{1-0.3} \right] = 0.357$

$r = \frac{A_0 - A}{A_0}$   $\bar{\sigma} = 500(0.357)^{0.5} = 299 \text{ MPa.}$

Q) (a) The strain-hardening behavior of an annealed low-carbon steel is approximated by  $\bar{\sigma} = 700 \bar{\epsilon}^{0.2}$

Estimate yield strength after bar is cold worked 50%.

(b) Suppose another bar of same steel was cold worked an unknown amount and then cold worked 15% more and found to have yield strength 525 MPa. What was the unknown amount of cold work?

Ans: (a) Strain was  $\ln \left( \frac{1}{1-0.5} \right) = 0.693$ ,  $\sigma = 700(0.693)^{0.2} = 650 \text{ MPa.}$

(b)  $\bar{\epsilon} = \left( \frac{\bar{\sigma}}{K} \right)^{1/n} = \left( \frac{525}{700} \right)^5 = 0.237$

15% cold work  $\approx \ln \left[ \frac{1}{1-0.15} \right] = 0.1625$

Hence unknown strain =  $0.237 - 0.1625 = 0.0745$

Calculate  $r = ?$

$\epsilon = \ln \frac{1}{1-r}$

$\Rightarrow \frac{1}{1-r} = e^\epsilon$

$\Rightarrow 1-r = \frac{1}{e^\epsilon}$

$\Rightarrow r = 1 - \frac{1}{e^\epsilon} = \frac{e^\epsilon - 1}{e^\epsilon}$

Q) An aluminum test specimen 100 mm long, 20 mm wide and 2 mm thick is elongated to 130 mm. If anisotropy ratio  $r = 2$ , determine transverse strain in length, width and thickness directions.

Ans: 
$$\frac{\epsilon_w}{\epsilon_t} = 2$$

$$\epsilon_L + \epsilon_w + \epsilon_t = 0$$

$$\Rightarrow 3\epsilon_t = -\epsilon_L = -\ln\left(\frac{130}{100}\right) = -0.262$$

$$\epsilon_t = -0.0873$$

$$\epsilon_w = 2 \times \epsilon_t = -0.1746$$

Q) The  $K$ ,  $n$  and  $m$  values for a stainless steel sheet are 1140 MPa, 0.35 and 0.01 respectively. A test piece has initial width, thickness and gauge length of 12.5, 0.45 and 50 mm respectively. Determine the increase in load when extension is 10% and the extension rate of gauge length is increased from 0.5 to 50 mm/min.

Ans: 
$$\sigma = K \epsilon^n \dot{\epsilon}^m$$

$$\epsilon = \ln\left(\frac{l}{l_0}\right) = \ln\left(\frac{55}{50}\right) = 0.0953$$

As  $l = 10\% \text{ ext. } 50 = 50 + \frac{50 \times 10}{100} = 55$

$$\dot{\epsilon}_1 = \frac{v_1}{L} = \frac{0.5 \times 10^{-3}}{60} \bigg/ (55 \times 10^{-3}) = 0.1515 \times 10^{-3} \text{ sec}^{-1}$$

$$\dot{\epsilon}_2 = \frac{v_2}{L} = \frac{50 \times 10^{-3}}{60} \bigg/ (55 \times 10^{-3}) = 15.15 \times 10^{-3} \text{ sec}^{-1}$$

$$\sigma_1 = K \epsilon^n \dot{\epsilon}_1^m = 459 \text{ MPa}$$

$$\sigma_2 = 480 \text{ MPa}$$

$$\Delta P = (\sigma_2 - \sigma_1) \cdot A = (\sigma_2 - \sigma_1) \cdot \frac{A_0 l_0}{L} = 0.27 \text{ kN}$$

Q1 A cylindrical test specimen of diameter 10mm and gauge length 50mm is extended to 65mm. Determine the true strain. Neglect elastic deformation. If the ultimate strength occurs at a force of 25000N and at an extension of 70mm, determine the strain hardening exponent  $n$  and ultimate strength of the material.

Ans:  
 true strain at 65mm =  $\epsilon = \ln \frac{65}{50} = 0.2623$

∴ true strain at 70mm =  $\epsilon_u = \ln \frac{70}{50} = 0.3364$

$\epsilon_u = n = 0.3364$

$\epsilon = \ln \left( \frac{l}{l_0} \right) = \ln \left( \frac{A_0}{A} \right)$

∴  $\frac{A_0}{A} = e^{\epsilon_u}$

∴  $A = \frac{A_0}{e^{\epsilon_u}} = \frac{\frac{\pi}{4} \times 10^2}{e^{0.3999}} = 56.104 \text{ mm}^2$

True ultimate strength =  $\frac{25000}{56.104} = 445.6 \text{ N/mm}^2$

∴  $\frac{25000}{\frac{\pi}{4} \times 10^2} = 318.31 \text{ N/mm}^2$

(4)

Q) A mild steel rectangular specimen of length 100mm. is extended to 120mm. Neglects elastic defmt. And takes the material as isotropic, determine the strain true strain in length, width and thickness.

$$\epsilon_L = \ln \frac{120}{100} = 0.1823$$

$$\epsilon_L + \epsilon_w + \epsilon_t = 0 \quad \Rightarrow \quad \epsilon_w = \epsilon_t = -\frac{1}{2} \epsilon_L$$

$$\epsilon_w = \epsilon_t = -0.09115$$

Q) Determine the true strain in length, width and thickness of sheet if specimen is elongated to 130% of its original length and because of anisotropy the ratio  $\epsilon_w/\epsilon_t = 1.5$ . Also determine % decrease in area of  $\epsilon_s$ .

$$\epsilon_L = \ln \frac{130}{100} = 0.2623$$

$$\frac{\epsilon_w}{\epsilon_t} = 1.5 \quad \epsilon_L + \epsilon_w + \epsilon_t = 0$$

$$\Rightarrow \epsilon_L + 1.5 \epsilon_t + \epsilon_t = 0$$

$$\Rightarrow 2.5 \epsilon_t = -\epsilon_L \Rightarrow \epsilon_t = -\frac{\epsilon_L}{2.5} = -0.1049$$

$$\text{and } \epsilon_w = 1.5 \epsilon_t = -0.1573$$

$$\text{due to plastic defmt } \frac{da}{a} = -\frac{dL}{L} = -30\%$$

⑤

Q1) Brass chaplets are used to support sand core inside a sand mold cavity. The projected core print area is  $13 \text{ cm}^2$  for each end of the cylindrical sand core which support at both ends. The design of the chaplets and the manner in which they are placed in the mold cavity surface allows each chaplet to sustain a force of  $45 \text{ N}$ . If the vol<sup>n</sup> of the core =  $7.5 \times 10^3 \text{ cm}^3$  and the metal poured is brass, determine the minimum number of chaplets that should be placed (a) beneath the core, and (b) above the core (Density of sand core and brass are  $1.6$  and  $8.67 \text{ gm/cm}^3$  respectively and the green sand strength is  $6.9 \times 10^3 \text{ N/m}^2$ ).

Ans: (a) The weight of the core =  $W_c = V_c \times \rho_c$

$$= \frac{7.5 \times 10^3}{1000} \times 1.6 \times 9.8 \text{ N}$$

$$= 117.6 \text{ N}$$

The support for core print =  $F_{cp} = 2 \times 6.9 \times 10^3 \times \frac{13}{10000} \times \frac{13}{10}$

$$= 17.94 \text{ N}$$

No of ~~cores~~ <sup>Chaplets</sup> required =  $\frac{W_c - F_{cp}}{F_{chap}} = \frac{117.6 - 17.94}{45}$

$$= 2.21 \approx \underline{\underline{3 \text{ nos}}}$$

(b) after pouring the liquid metal the buoyancy force. ~~(net force)~~

$$= V_c \times (\rho_L) \times g$$

Net force =  $V_c \times (\rho_L - \rho_c) \times g = \frac{7.5 \times 10^3}{1000} \times (8.67 - 1.6) \times 9.8$

$$= 519.65 \text{ N}$$

⑥

$$\text{Support f - Core print} = 17.94$$

$$\text{No of chuplets at top} = \frac{519.65 - 17.94}{45}$$

$$= 11.15 \approx 12 \text{ Nos}$$

Ans:

(7)

$$\Delta T = 236^\circ\text{C}$$

$$T_E = 1085 + 273 = 1358^\circ\text{K}$$

$$L = 1628 \text{ J/cm}^3$$

$$r = 177 \times 10^{-7} \text{ J/cm}^2$$

$$r^* = \frac{2rT_E}{L\Delta T} = \frac{2 \times (177 \times 10^{-7}) \times (1358)}{(1628) \times (236)}$$

$$= 12.51 \times 10^{-8} \text{ cm}$$

Lattice parameter of FCC copper  $a = 0.3615 \text{ nm}$   
 $= 3.615 \times 10^{-8} \text{ cm}$

Volume of unit cell  $= a^3 = (3.615 \times 10^{-8})^3 = 47.24 \times 10^{-24} \text{ cm}^3$

The number of unit cells in the critical nucleus is

$$= \frac{\text{Voln of critical nucleus}}{\text{Voln of unit cell}}$$

$$= \frac{\left(\frac{4}{3} \pi r^3\right)}{47.24 \times 10^{-24}} = \frac{\frac{4}{3} \times \pi \times (12.51 \times 10^{-8})^3}{47.24 \times 10^{-24}}$$

$$= 174 \text{ unit cells}$$

Therefore, for atoms in each unit cell.

No of atoms in the critical nucleus  $= 4 \times 174 = 696$   
 atoms

Ans:  $\Delta T = 480^\circ\text{C}$

③

$$r^* = \frac{2\gamma T_E}{L \Delta T}$$

$$T_E = 1453 + 273 = 1726^\circ\text{K}$$

$$L = 2756 \text{ J/cm}^3$$

$$\gamma = 255 \times 10^{-7} \text{ J/cm}^2$$

$$r^* = \frac{2\gamma T_E}{L \Delta T} = \frac{2(255 \times 10^{-7})(1726)}{(2756)(480)}$$

$$= 6.654 \times 10^{-8} \text{ cm.}$$

Volume of Nucleus =  $\frac{4}{3}\pi r^{*3} = \frac{4}{3}\pi \times (6.654 \times 10^{-8})^3$

Lattice parameter of FCC Nickel =  $a = 0.356 \text{ nm} = 0.356 \times 10^{-9} \text{ m}$   
 $= 0.356 \times 10^{-7} \text{ cm}$   
 $= 3.56 \times 10^{-8} \text{ cm}$

$$V_{\text{unit cell}} = a^3 = (3.56 \times 10^{-8})^3 = 45.11 \times 10^{-24} \text{ cm}^3$$

$$\text{No of unit cell} = \frac{\frac{4}{3}\pi \times (6.654)^3 \times 10^{-24}}{45.11 \times 10^{-24}}$$

$$= \frac{4 \times \pi \times (6.654)^3}{3 \times 45.11} = 27.356$$

Contact angle related to Lattice mismatch.  $\theta = \frac{\Delta a}{a}$

$a$  is lattice parameter of crystal.  $v_c = \frac{\Delta a}{a} = 0.014$

for Al  $\rightarrow T_{ic} = \frac{\Delta a}{a} = 0.060$   $T_{iB_2} = \frac{\Delta a}{a} = 0.048$

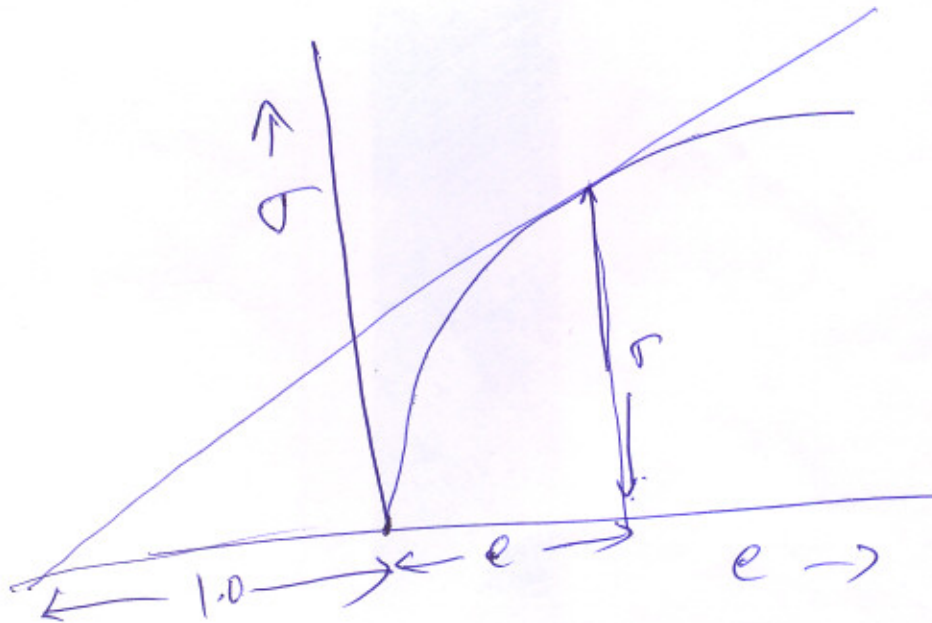


$$\frac{d\sigma}{d\epsilon} = \sigma$$

$$\begin{aligned} \epsilon_1 + \epsilon_2 + \epsilon_3 &= 0 \\ \ln(1+\epsilon_1) + \ln(1+\epsilon_2) + \ln(1+\epsilon_3) &= 0 \\ \ln(1+\epsilon_1)(1+\epsilon_2)(1+\epsilon_3) &= 0 \\ \Rightarrow (1+\epsilon_1)(1+\epsilon_2)(1+\epsilon_3) &= 1 \end{aligned}$$

$$\begin{aligned} \epsilon &= \ln(1+e) \\ d\epsilon &= \frac{de}{1+e} \end{aligned}$$

$$\frac{d\sigma}{de} = \frac{\sigma}{1+e}$$



The following data pairs (load kN, extension mm) were obtained from plastic part of the load extension file of a tensile test of extra deep draw quality steel of 0.8mm thickness. The initial test piece width was 12.5mm and gauge length was 50mm.

1.57, 0.080 : 1.90, 0.760 : 2.24, 1.85 : 2.57, 3.66 :

2.78, 5.84 : 2.90, 8.92 : 2.93, 11.06 : 2.94, 13.49 :

2.92, 16.59 : 2.86, 19.48 : 2.61, 21.82 : 2.18, 22.69

obtain, elongation strain, true stress - true strain, UTS,  $f_u$ , total elongation %, K value, n-value.

Q16 Determine the work done if a bar of 10mm diam and 200mm length is elongated by 22mm. The yield strength of the material of specimen is given as  $\sigma = 250 \cdot \epsilon^{0.3}$  N/mm<sup>2</sup>.  
(Neglect elastic deflection)

(Ans 158.38 Nm)